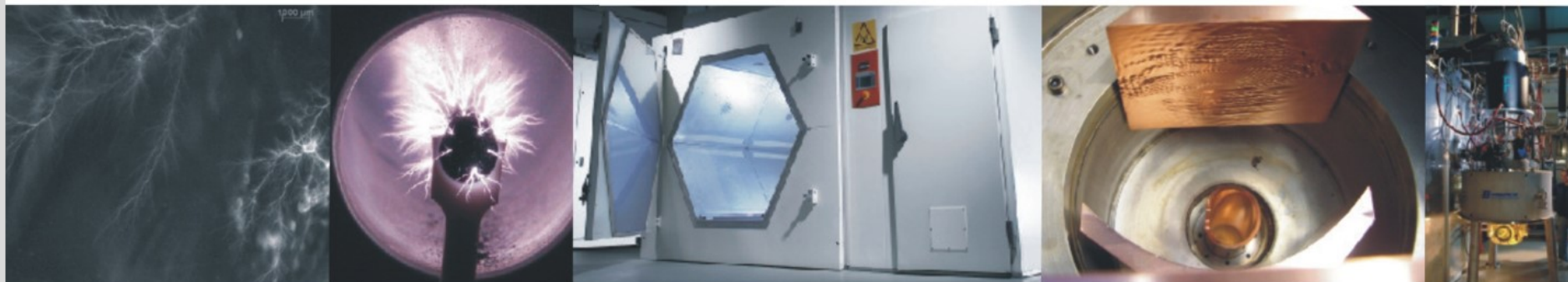


Study of Very High-Order Volume Modes as Possible Alternatives to the TE_{34,19} Operating Mode of the KIT 2 MW 170 GHz Coaxial-Cavity Gyrotron

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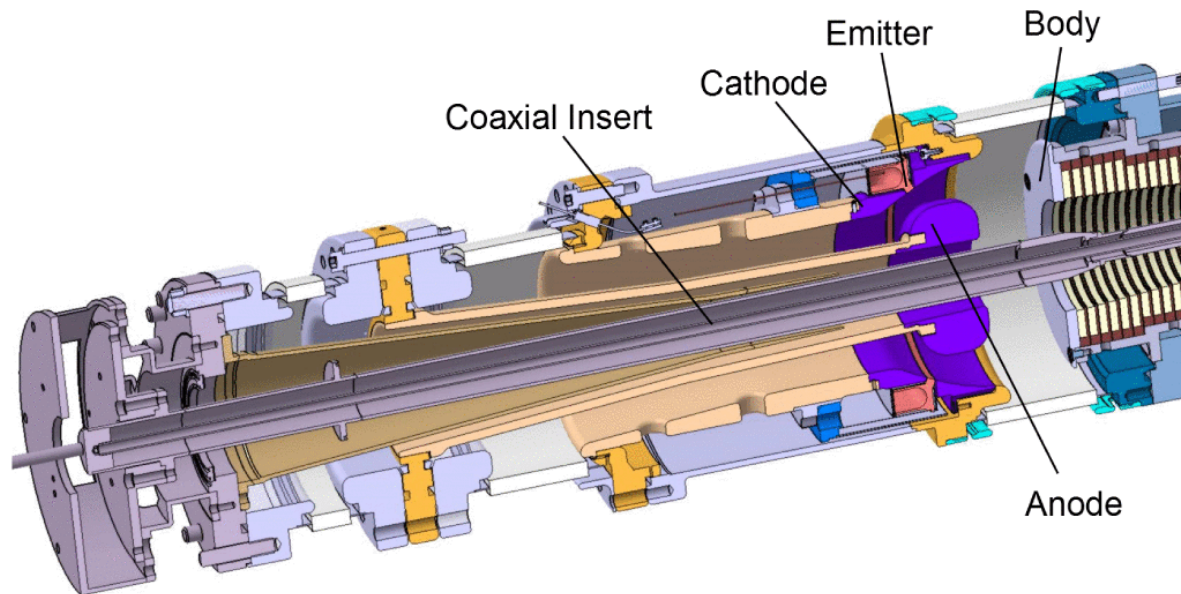
Outline

- Introduction
- State of the art: The $TE_{34,19}$ operating mode
 - Basic operational parameters
 - Startup simulation
- The $TE_{25,22}$ operating mode as possible alternative operating mode
 - Basic operational parameters
 - Startup simulation
 - Cavity geometry comparison
 - Thermal simulation of coaxial insert
 - $TE_{25,22}$ geometry at 204 GHz
- $TE_{25,22}$ mode: Conclusion

Motivation

The gyrotron design for the KIT 170 GHz 2 MW coaxial-cavity gyrotron, can be downsized by 25 %. Achieved by downsizing the IMIG.

- **Decrease of warm bore of SC magnet and e-beam radius by 25 %**
- **Significant decrease in overall gyrotron size and cost**



→ Find a high-order operating mode, which corresponds to this significantly smaller electron beam radius ($R_{beam} = 7.4 \text{ mm}$)

Constraints in the Mode Selection

- Mode selection is directed by the two main constraints:

Thermal Constraints	Operational Constraints
<ul style="list-style-type: none"> - Coaxial insert (0.2 kW/cm²) - Cavity walls (2.5 kW/cm²) 	<ul style="list-style-type: none"> - A mode with optimal mode stability and efficiency has to be selected. - Maximal beam current and acceleration voltage are determined by the limitations of the HV power supply

- The Eigenvalue (χ_c) of the selected mode should be close to the χ_c of the TE_{34,19} operating mode, in order to achieve similar mode stability.
- The operating frequency is ≈ 170 GHz
- The coaxial cavity for this mode
 - has to be manufacturable, and
 - has to provide enough space for the cooling system.

→ TE_{25,22} operating mode

$TE_{34,19}$ OPERATING MODE AS A REFERENCE OPERATING MODE

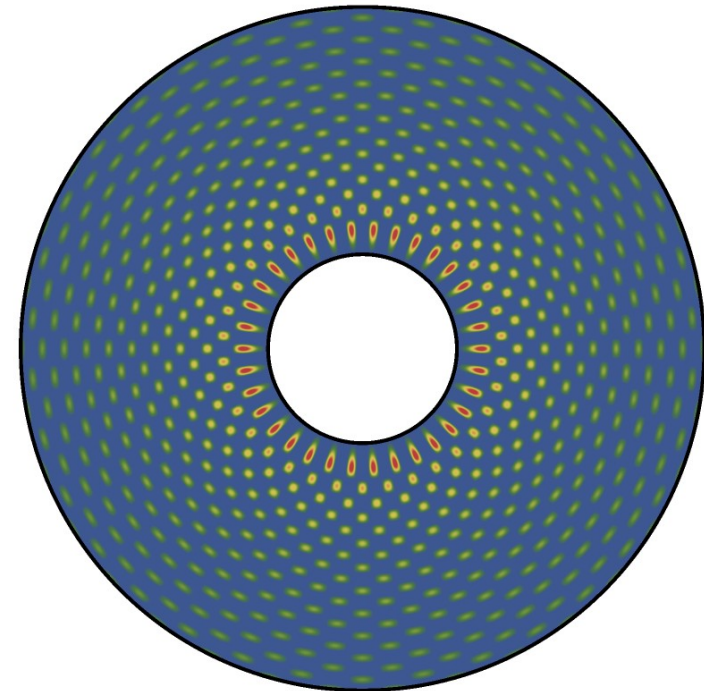
TE_{34,19} Mode Overview

Input Parameters

- $\chi_c \approx 105.19296$
- $R_{beam} = 10 \text{ mm}$
- $R_{out} = 29.550 \text{ mm}$
- $R_{in} = 8.0 \text{ mm}$
- $U_{cath} = 90.0 \text{ kV}$
- $I_{beam} = 75 \text{ A}$

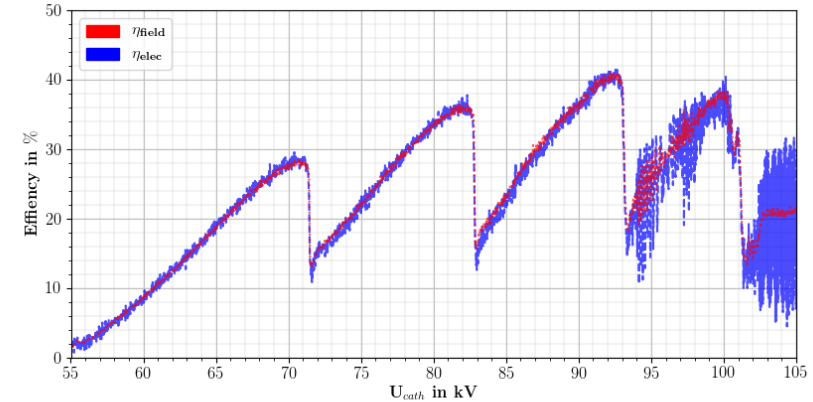
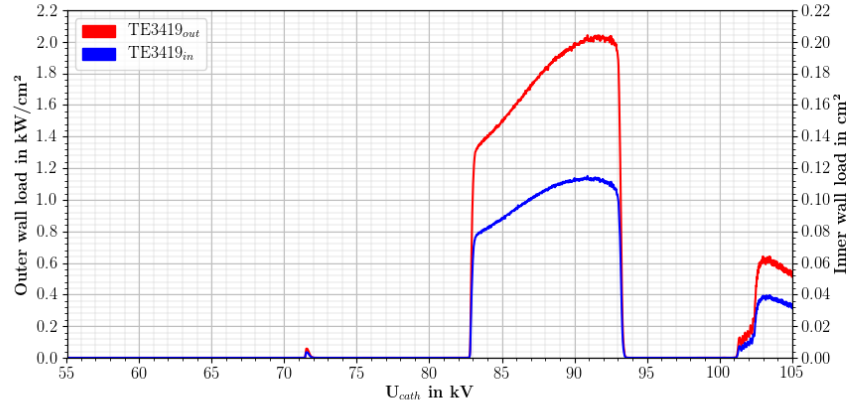
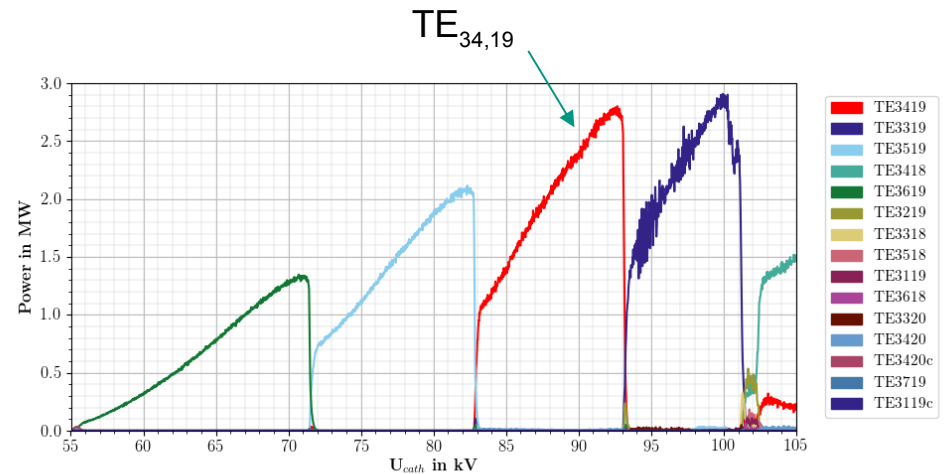
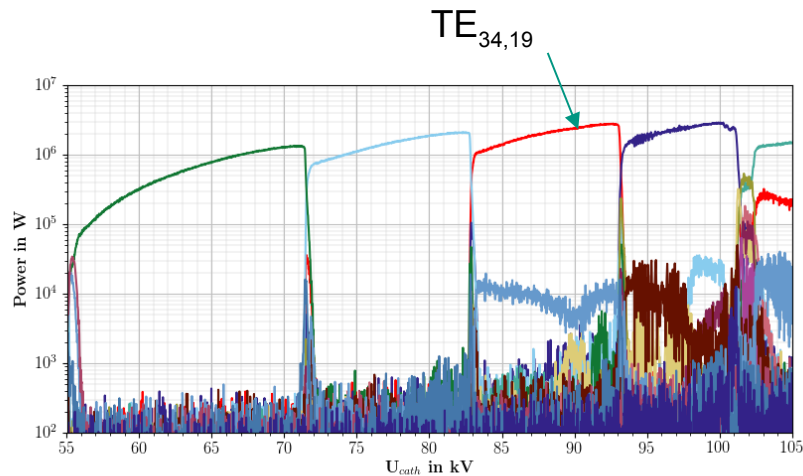
Simulation Results

- $P_o = 2.5 \text{ MW}$
- $\rho_{out} = 2.0 \text{ kW/cm}^2$
- $\rho_{in} = 0.12 \text{ kW/cm}^2$
- $\eta_{elec} = 37 \%$



H_z of the TE_{34,19} operating mode (non-rotating)

Reference Simulation (TE_{34,19} Operating Mode)



TE_{34,19} has an output power of 2.5 MW at 90 kV. The mode is lost at 93 kV. Electron and field efficiency coincide. $\eta_{elec} = 37\%$ at 90 kV. Field and electron efficiency coincide.

THE NEW $TE_{25,22}$ OPERATING MODE

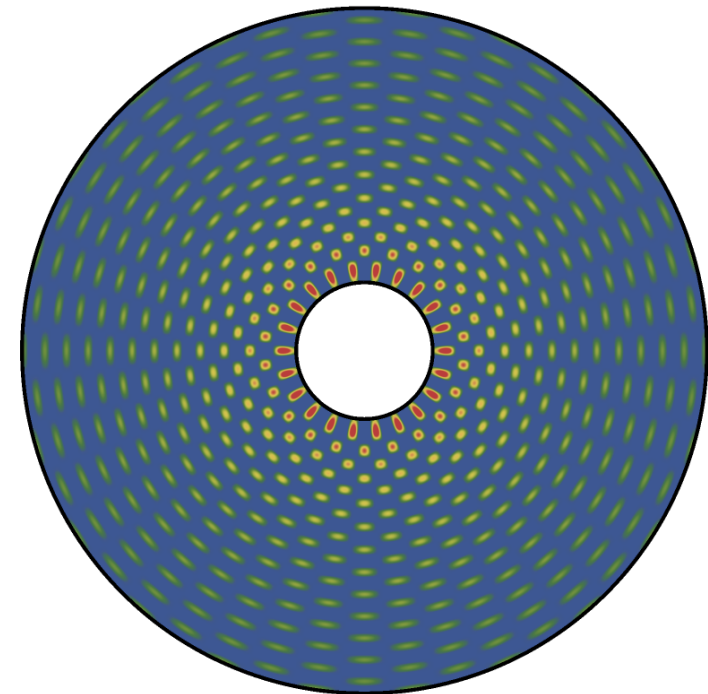
TE_{25,22} Mode Overview

■ New Input Parameters

- $\chi_c \approx 102.44572$
- $R_{beam} = 7.4 \text{ mm}$
- $R_{out} = 28.90 \text{ mm}$
- $R_{in} = 5.65 \text{ mm}$
- $U_{cath} = 90.0 \text{ kV}$
- $I_{beam} = 75 \text{ A}$

■ Simulation Results

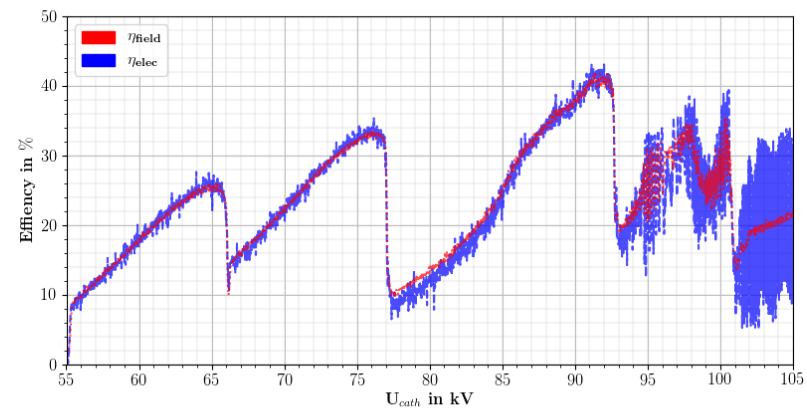
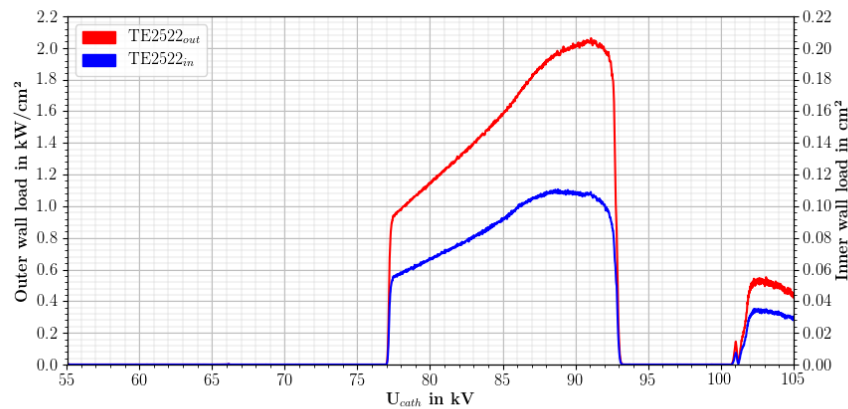
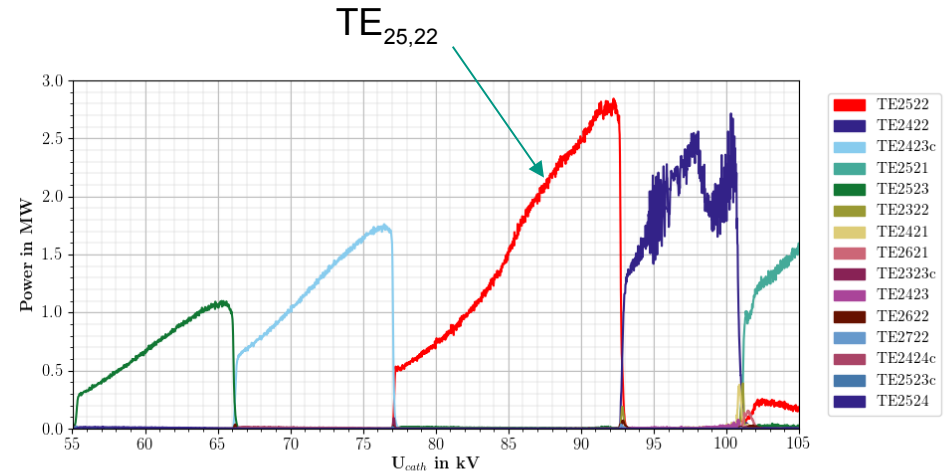
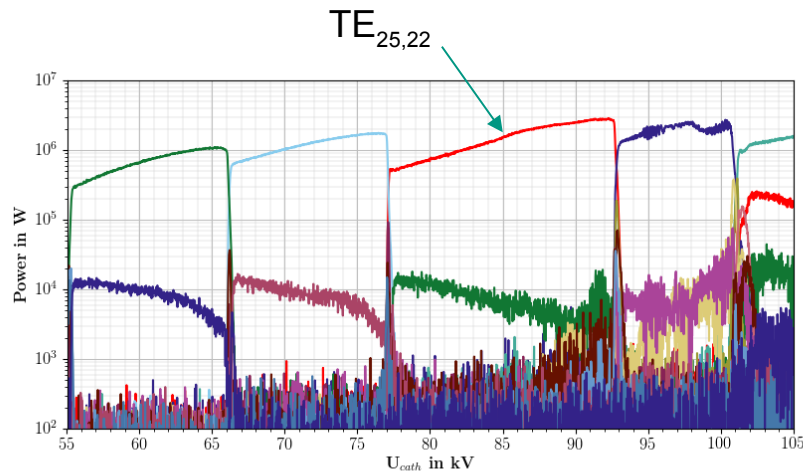
- $P_o = 2.5 \text{ MW}$
- $\rho_{out} = 2.0 \text{ kW/cm}^2$
- $\rho_{in} = 0.11 \text{ kW/cm}^2$
- $\eta_{elec} = 37 \%$



H_z of the TE_{25,22} operating mode

The TE_{25,22} mode can be operated with the reduced beam radius. Simulation shows outputs parameters close to the TE_{34,19} mode

Simulation (TE_{25,22} Operating Mode)

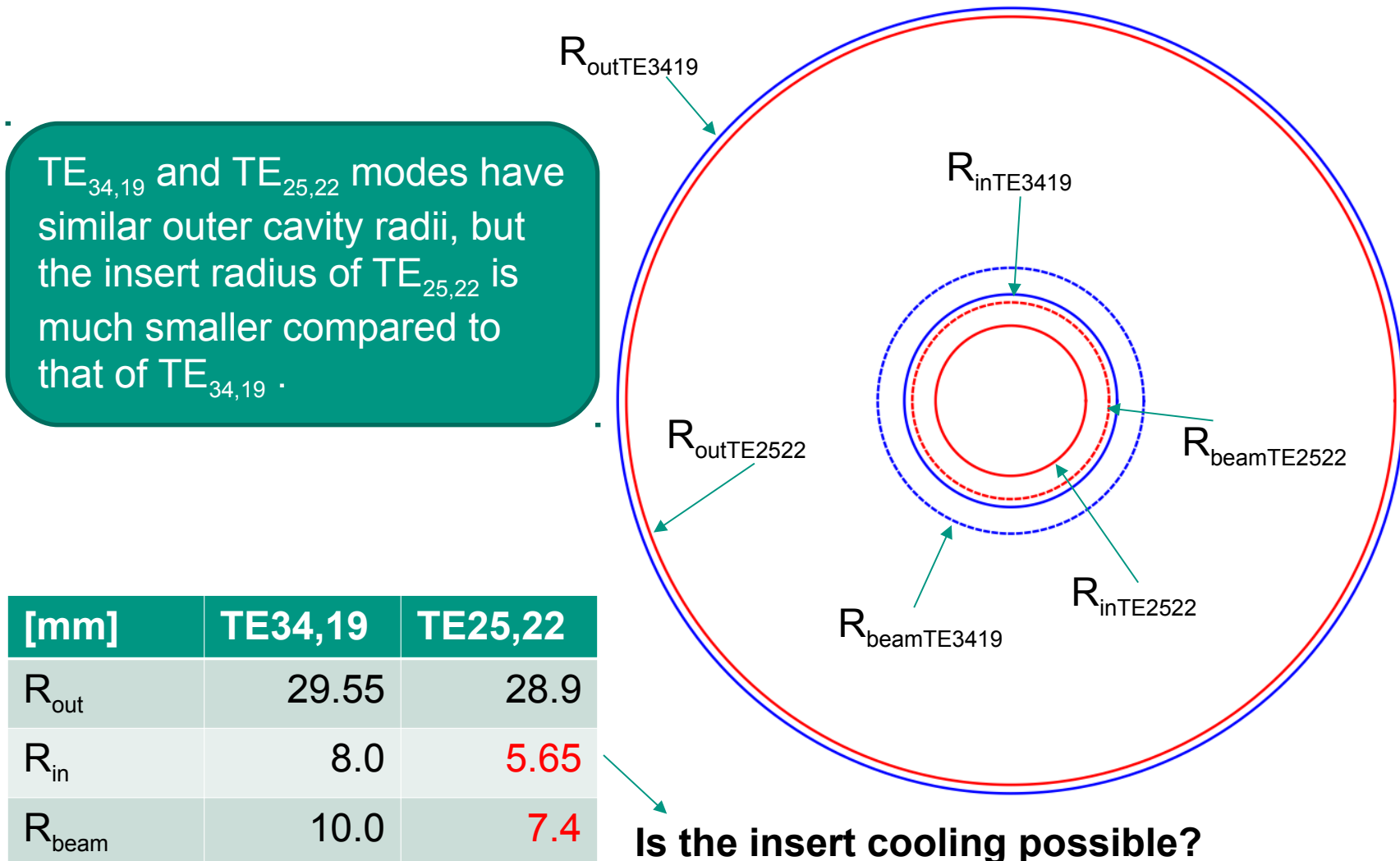


TE_{25,22} shows a stable startup with an output power of 2.5 MW. Mode is lost at 93 kV. η_{elec} = 37 % at 90 kV. Field and electron efficiency coincide!

CAVITY GEOMETRIES OF THE MODES $TE_{34,19}$ AND $TE_{25,22}$

Comparison of the Cavity Cross Section for the Modes $TE_{34,19}$ and $TE_{25,22}$

$TE_{34,19}$ and $TE_{25,22}$ modes have similar outer cavity radii, but the insert radius of $TE_{25,22}$ is much smaller compared to that of $TE_{34,19}$.

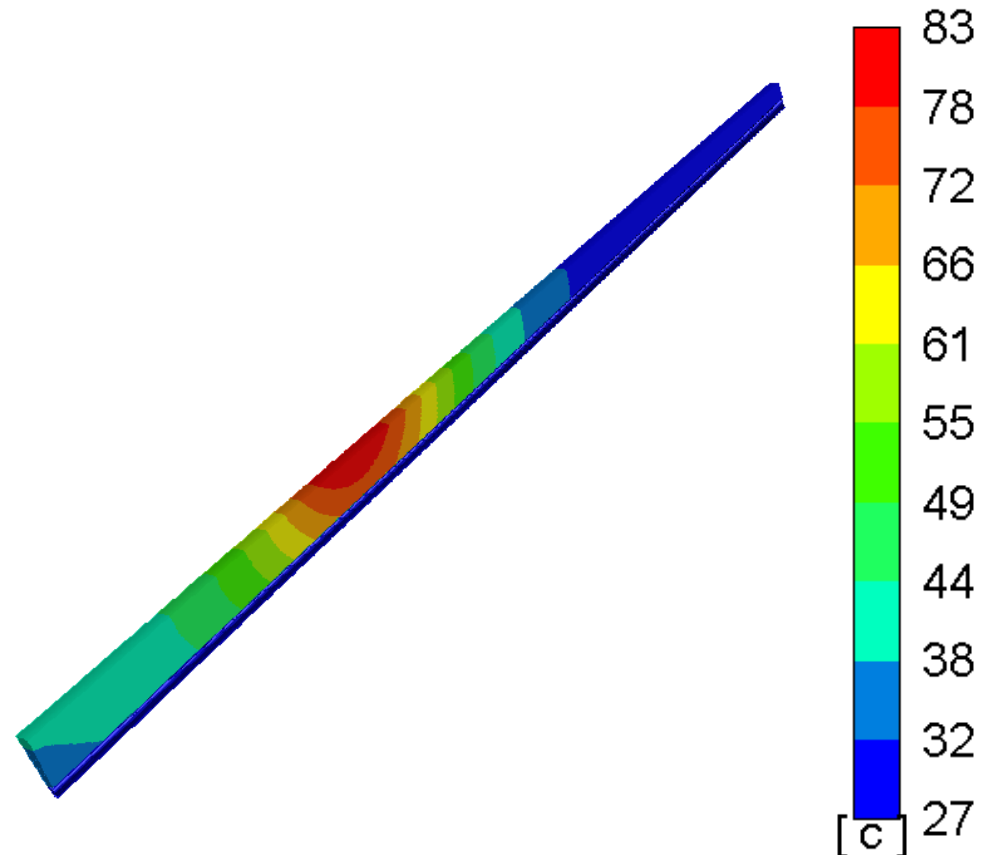


Is the insert cooling possible?

THERMAL SIMULATION OF THE INSERT FOR THE $TE_{25,22}$ OPERATING MODE

Thermal Load on the Coaxial Insert (TE_{25,22})

Simulation of the coaxial insert using „*Ansys fluent V 18.1 – Thermal-Hydraulic simulation*” shows no critical temperature on the insert.



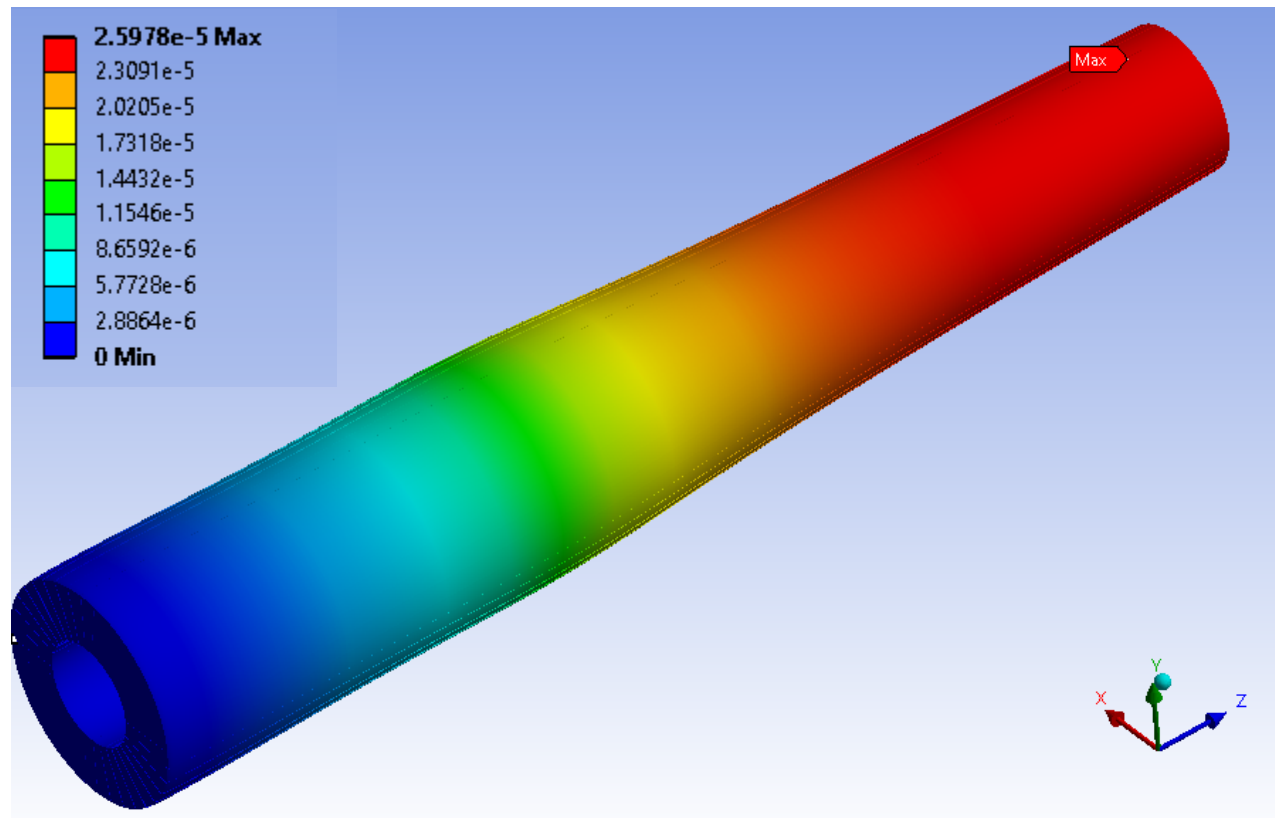
Temperatur profile along the coaxial insert

Simulation parameters

Water velocity	5.89 m/s
Mass-flow rate	4.37 L/min

Thermal Deformation of the Coaxial Insert (TE_{25,22})

Simulation of the coaxial insert using „Ansys mechanical - static-structural simulation” yields a maximum deformation of **2.6 μm** , which is negligible.



Deformation of the coaxial insert

**OPERATION OF
 $TE_{25,22}$ MODE CAVITY (170 GHz)
AT 204 GHz
→ $TE_{30,26}$ OPERATING MODE**

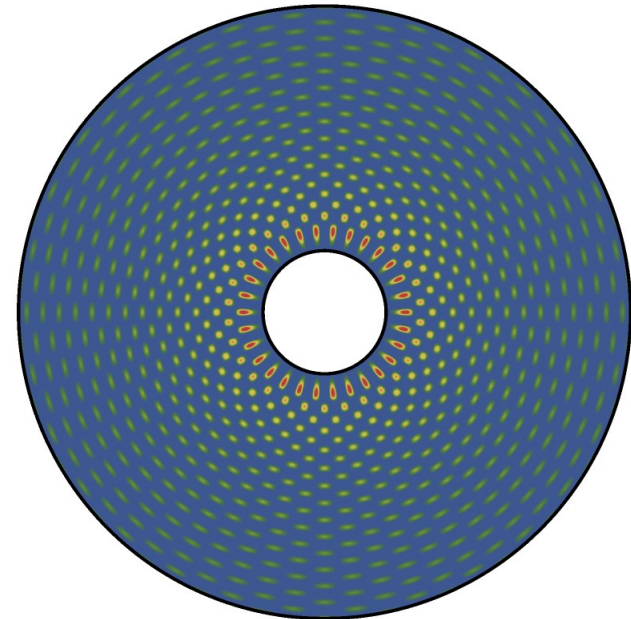
TE_{30,26} Mode Overview

Input Parameters

- $\chi_c \approx 122.76158$
- $R_{beam} = 7.42 \text{ mm}$
- $R_{out} = 28.90 \text{ mm}$
- $R_{in} = 5.65 \text{ mm}$
- $U_{cath} = 83.0 \text{ kV}$
- $I_{beam} = 70 \text{ A}$

Simulation Results

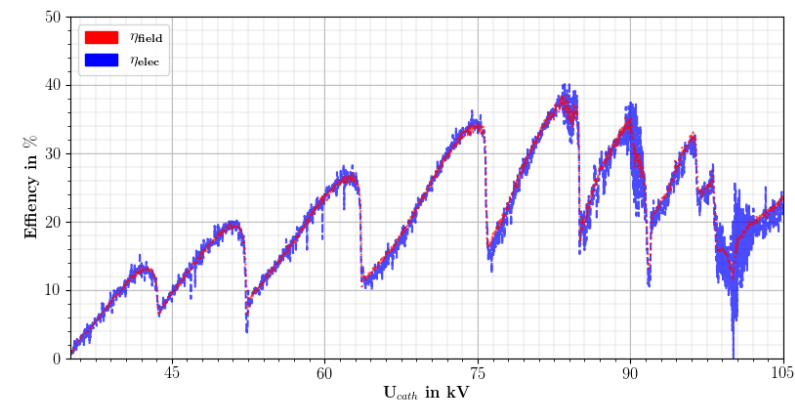
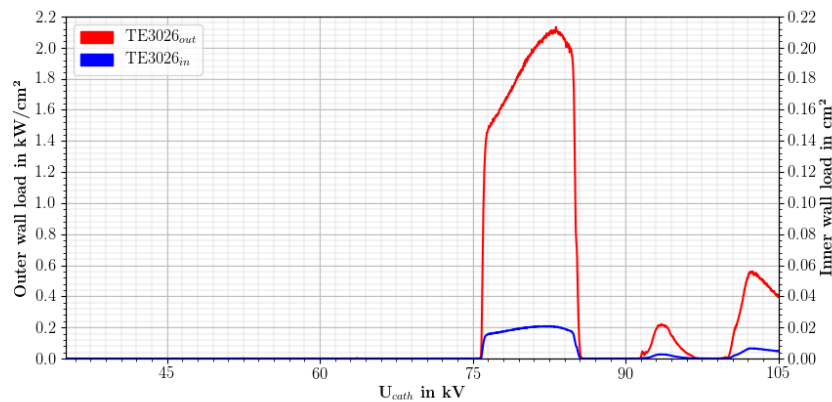
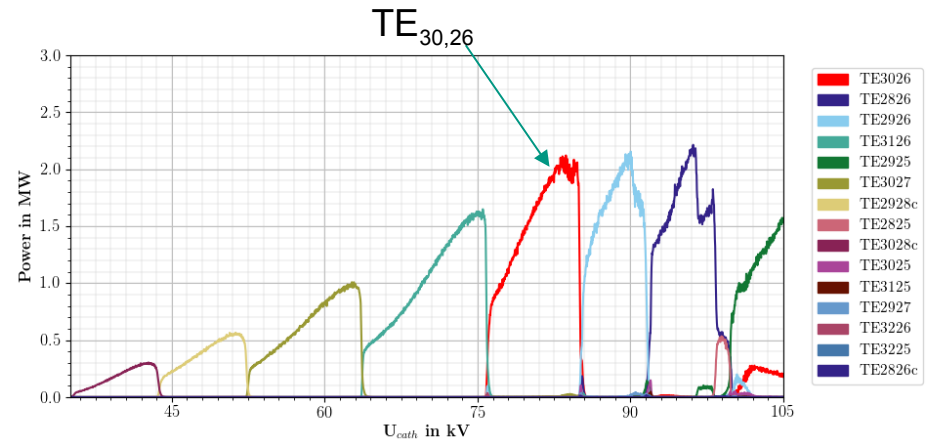
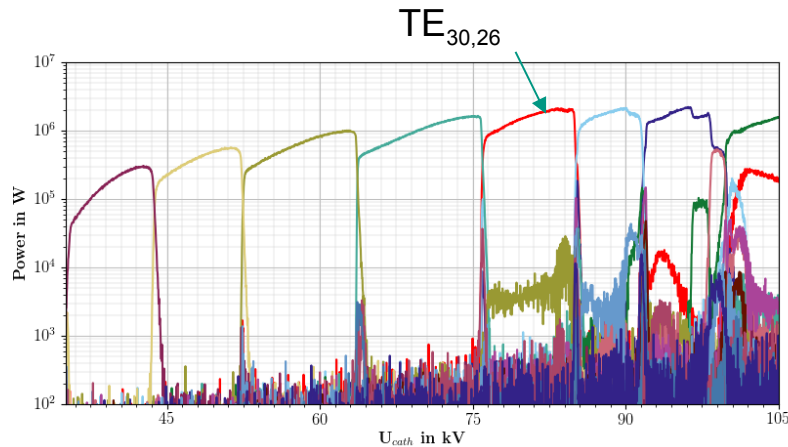
- $P_o = 1.8 \text{ MW}$
- $\rho_{out} = 2.2 \text{ kW/cm}^2$
- $\rho_{in} = 0.02 \text{ kW/cm}^2$
- $\eta_{elec} = 36 \%$



H_z of the TE_{30,26} operating mode

TE_{30,26} mode at 204 GHz corresponds to the TE_{25,22} mode at 170 GHz.

Simulation (TE_{30,26} Operating Mode)



TE_{30,26} mode shows good performance, but has stability problems due to mode competition with the mode TE_{30,27}. Mode is lost at 85 kV.

SUMMARY

Summary: $TE_{25,22}$ mode versus $TE_{34,19}$ mode

■ Advantages of the $TE_{25,22}$ Operating Mode

- Generates a high output power of **2.5 MW**
→ even higher output powers are possible (2.8 MW)
- Cooling of the the cavity is unproblematic
- An operation of the cavity at 204 GHz is possible
- Reduction of warm SC magnet bore hole by 25%
→ **Significant cost reduction for the magnet (at least 25 %)**

■ Future Tasks

- Sensitivity of the coaxial insert to mechanical vibrations, caused by the cooling liquid has to be checked
- Key components like uptaper and launcher have to be designed

Thank you for your attention

Please ask questions!

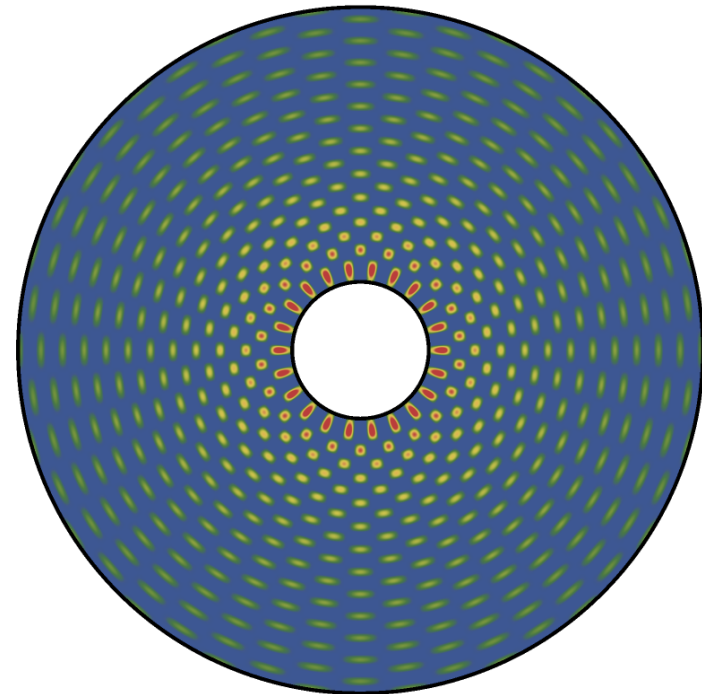
TE_{25,22} Overview

Input parameters

- $\chi_c \approx 102.44572$
- $R_{beam} = 7.4 \text{ mm}$
- $R_{out} = 28.90 \text{ mm}$
- $R_{in} = 5.65 \text{ mm}$
- $U_{cath} = 90.0 \text{ kV}$
- $I_{beam} = 85 \text{ A}$

Results

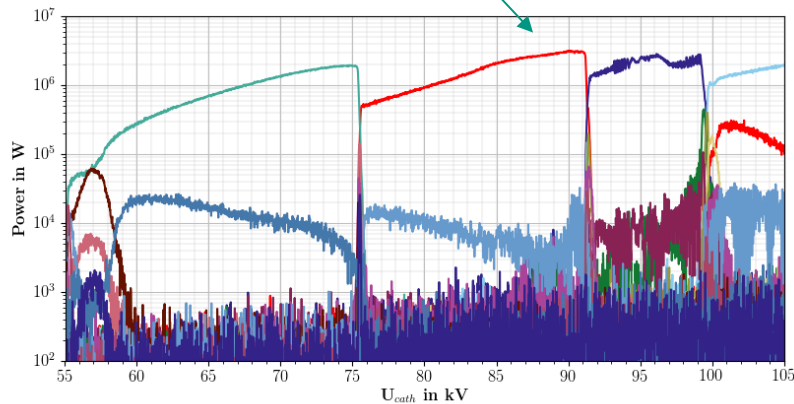
- $P_o = 2.8 \text{ MW (2.5)}$
- $\rho_{out} = 2.2 \text{ kW/cm}^2 (2.0)$
- $\rho_{in} = 1.4 \text{ kW/cm}^2 (0.12)$
- $\eta_{elec} = 38 \% (37)$



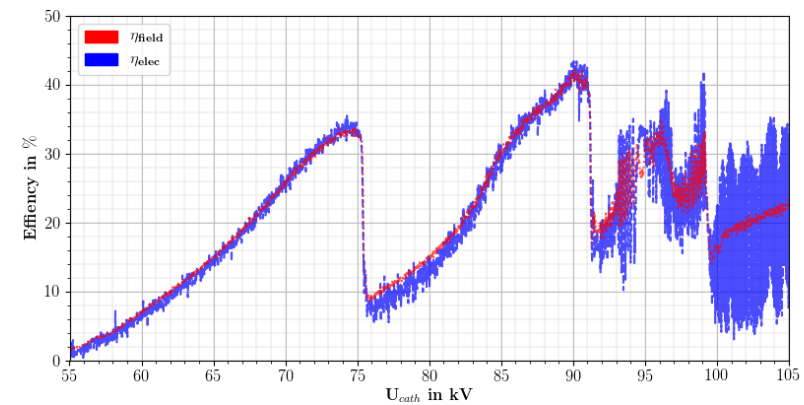
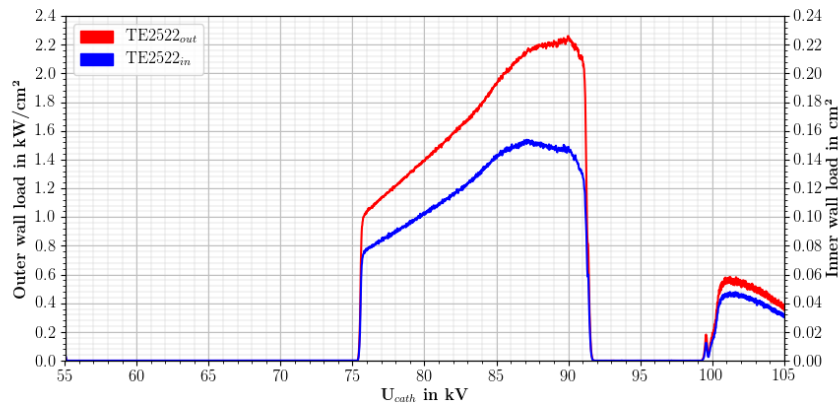
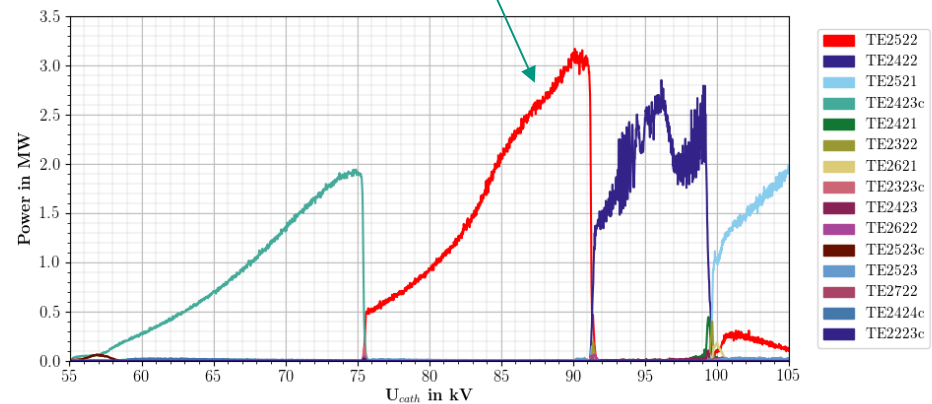
H_z of the TE_{25,22} operating mode

Simulation (TE_{25,22} Operating Mode) $I_{\text{beam}} = 85 \text{ A}$

TE_{25,22}



TE_{25,22}



TE_{25,22} is able to produce **2.8 MW** output power with a beam current of **85 A**. Mode stability is not affected and thermal loads are well below the limits and can be cooled.